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Wang et al.

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(54) **TRIBOELECTRIC NANOGENERATOR**

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(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 705 days.

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Related U.S. Application Data

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(51) **Int. Cl.**
H02N 1/04 (2006.01)

(52) **U.S. Cl.**
CPC **H02N 1/04** (2013.01)

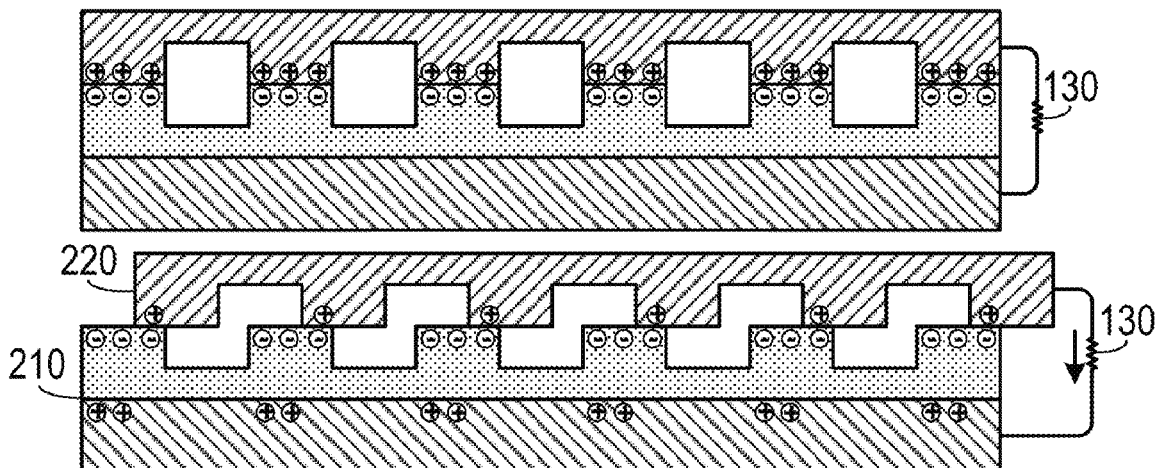
(58) **Field of Classification Search**
USPC 310/300, 309, 310; 200/181; 322/2 A;
318/116

See application file for complete search history.

(57) **ABSTRACT**

A generator includes a first member, a second member and a sliding mechanism. The first member includes a first electrode and a first dielectric layer affixed to the first electrode. The first dielectric layer includes a first material that has a first rating on a triboelectric series. The second member includes a second material that has a second rating on the triboelectric series that is different from the first rating. The second member includes a second electrode. The second member is disposed adjacent to the first dielectric layer so that the first dielectric layer is disposed between the first electrode and the second electrode. The sliding mechanism is configured to cause relative lateral movement between the first member and the second member, thereby generating an electric potential imbalance between the first electrode and the second electrode.

8 Claims, 6 Drawing Sheets



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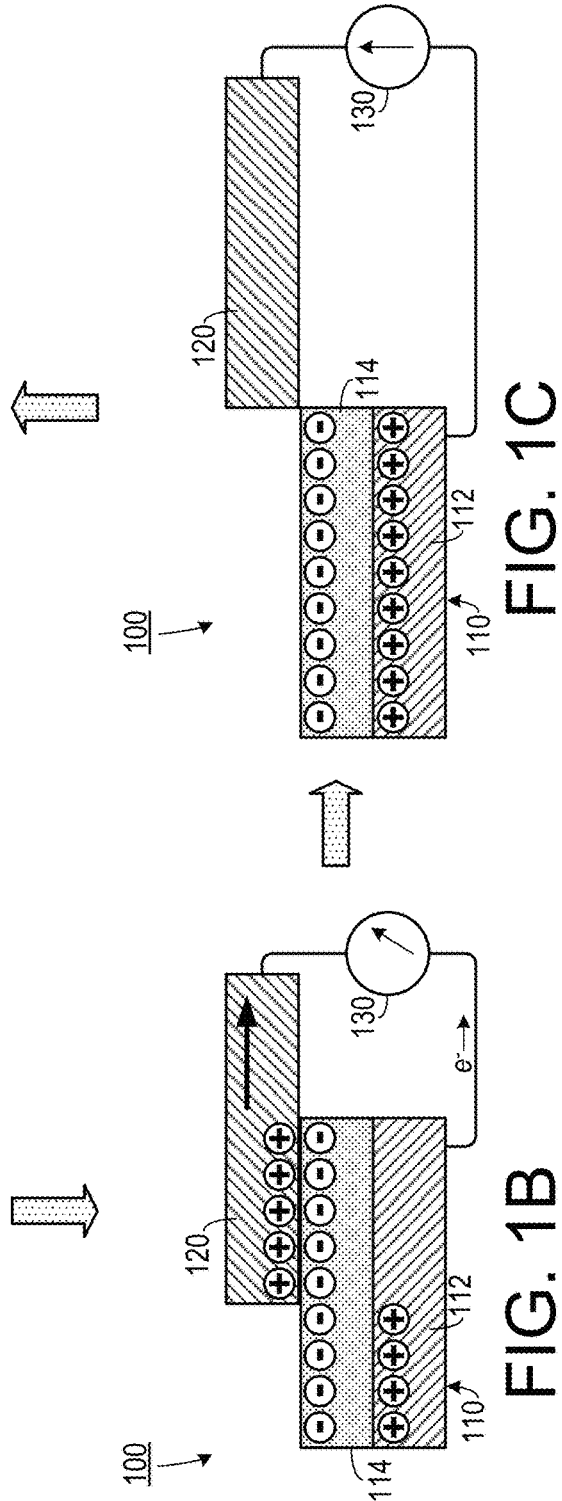
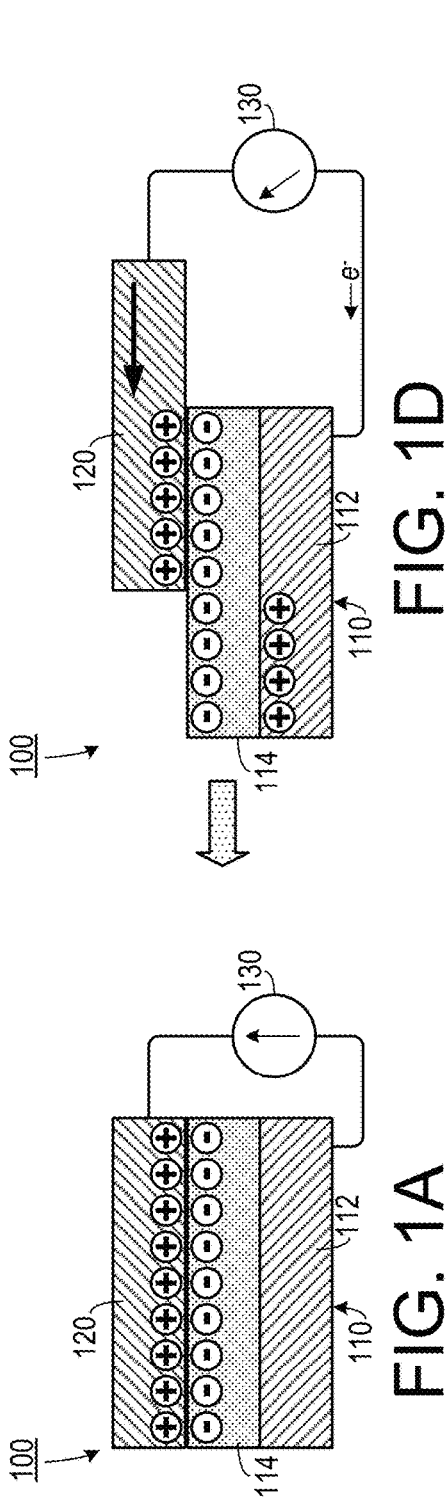
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Notification of Related Application: U.S. Appl. No. 13/598,132, filed Aug. 29, 2012 by Wang et al. and commonly owned by the assignee of the present application includes subject matter related to the present application.

Notification of Related Application: U.S. Appl. No. 14/032,864, filed Sep. 20, 2013 by Wang et al. and commonly owned by the assignee of the present application includes subject matter related to the present application.

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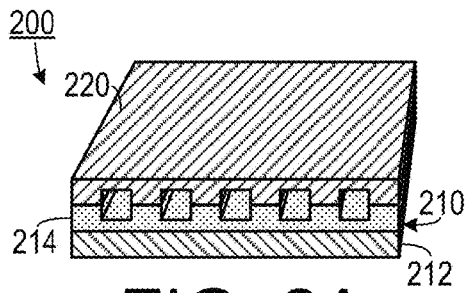


FIG. 2A

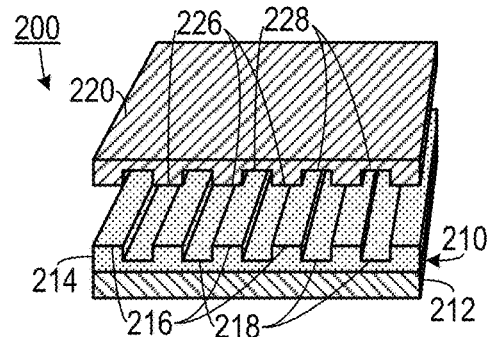


FIG. 2B

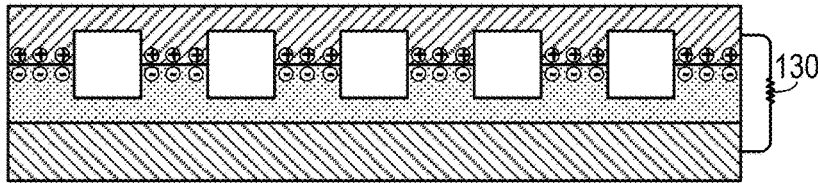


FIG. 3A

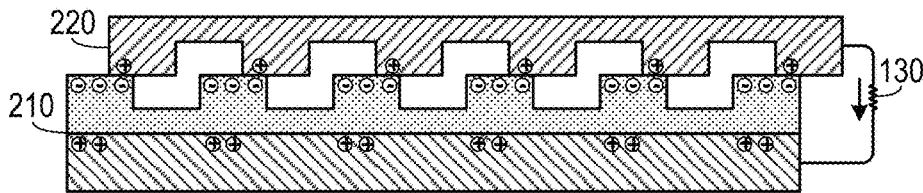


FIG. 3B

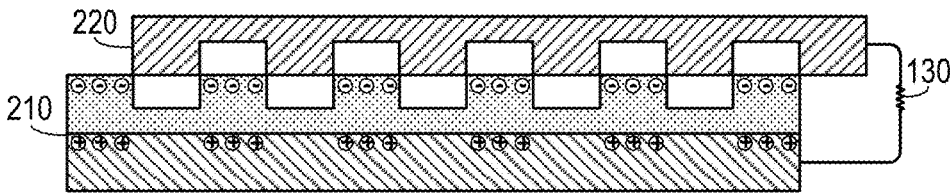


FIG. 3C

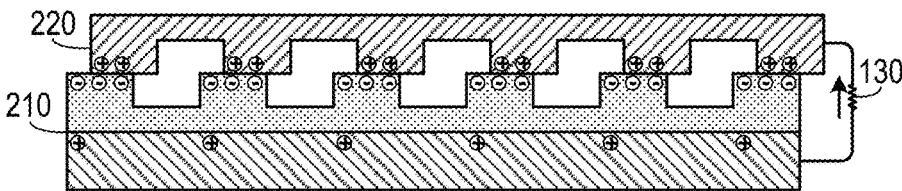


FIG. 3D

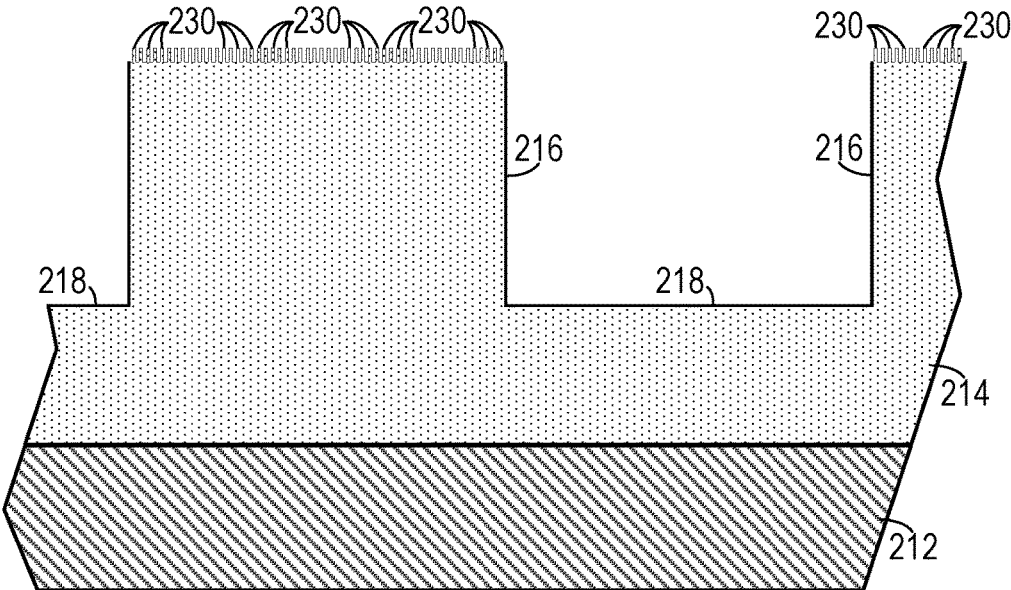


FIG. 2C

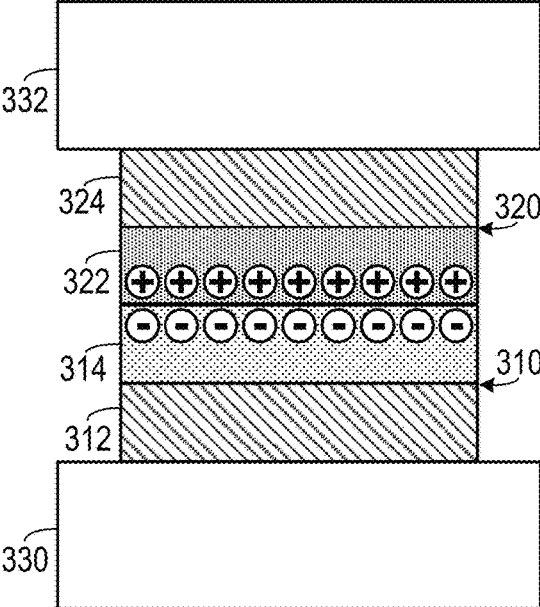


FIG. 4A

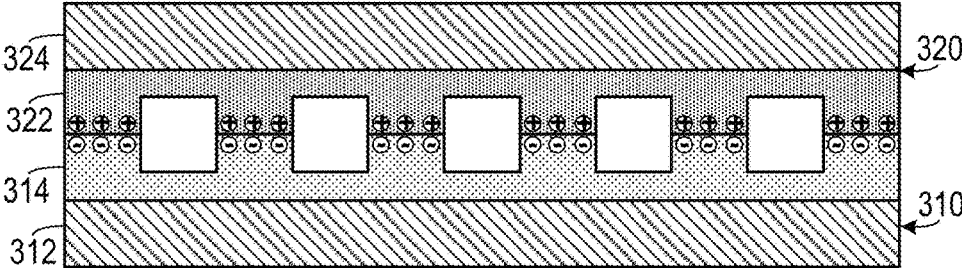


FIG. 4B

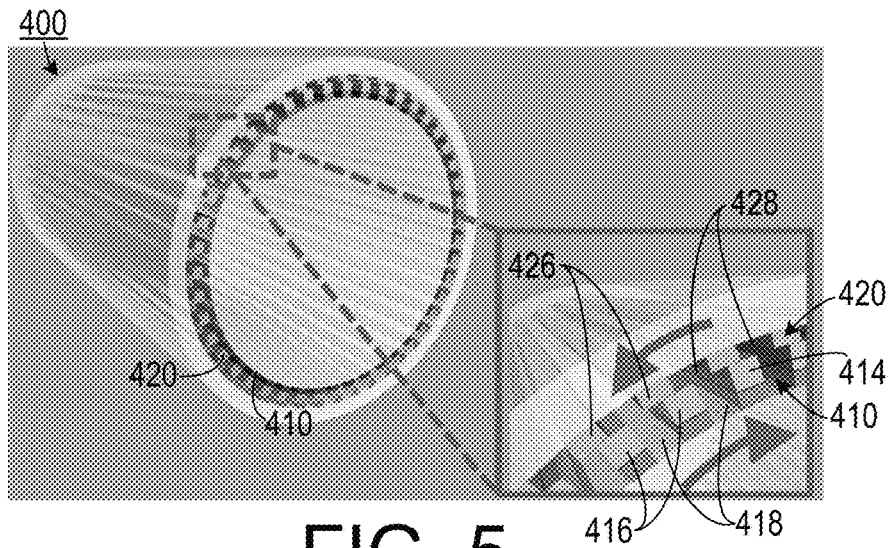


FIG. 5

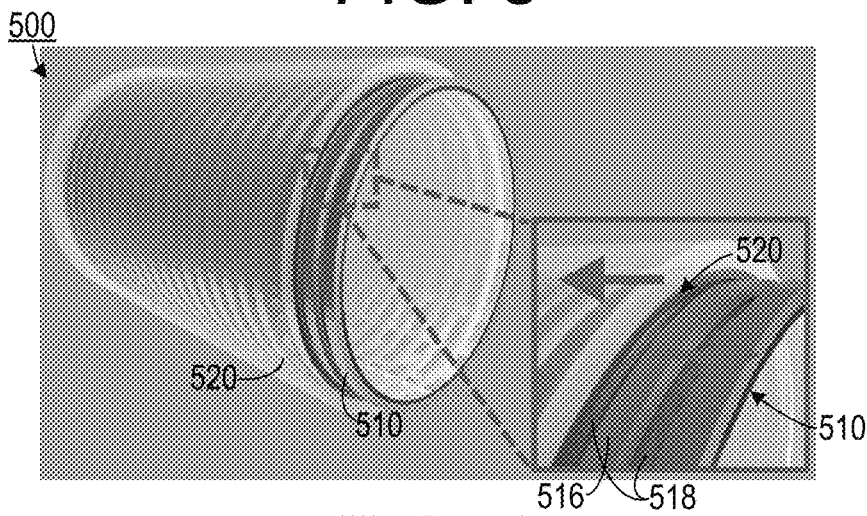


FIG. 6

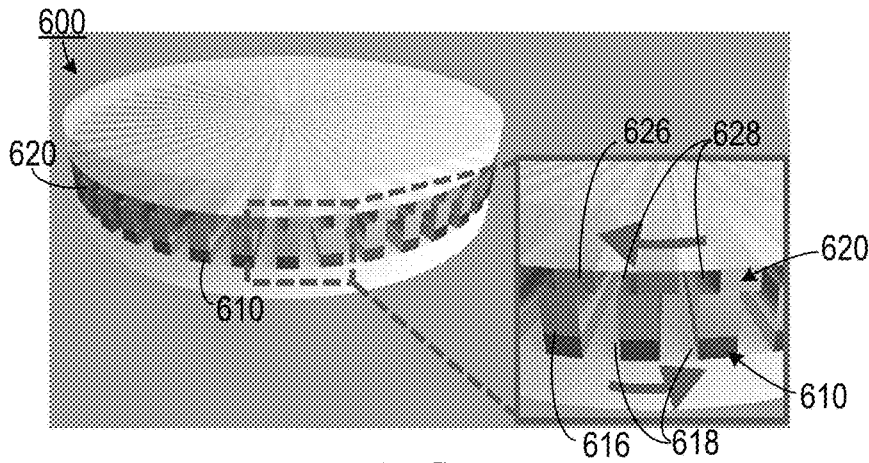


FIG. 7

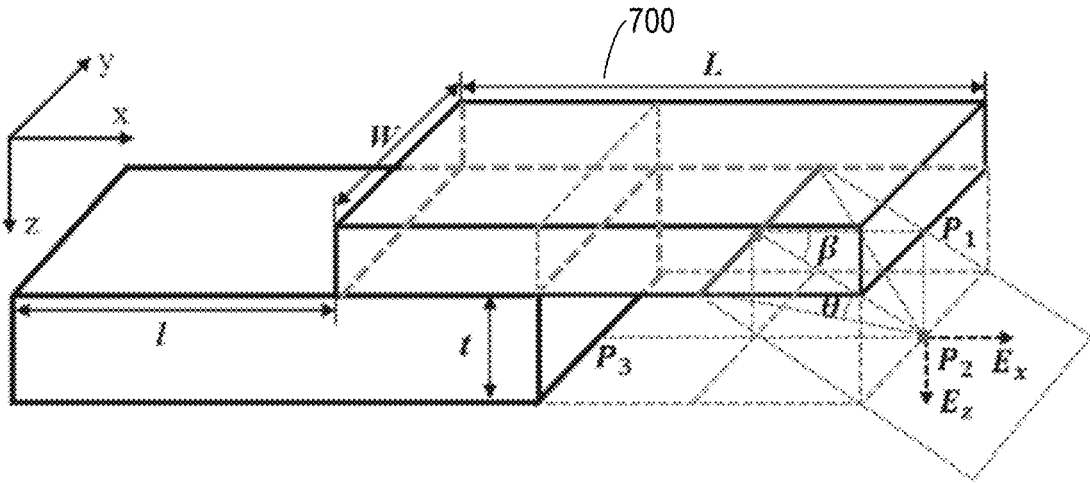


FIG. 8

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TRIBOELECTRIC NANOGENERATORCROSS-REFERENCE TO RELATED
APPLICATION(S)

This application claims the benefit of U.S. Provisional Patent Application Ser. No. 61/771,371, filed Mar. 1, 2013, the entirety of which is hereby incorporated herein by reference.

STATEMENT OF GOVERNMENT INTEREST

This invention was made with government support under agreement No. DE-FG02-07ER46394, awarded by the Department of Energy. The government has certain rights in the invention.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to generators and, more specifically, to a system for generating voltage and current using the triboelectric effect.

2. Description of the Related Art

Energy harvesting by converting ambient energy into electricity may offset the reliance of small portable electronics on traditional power supplies, such as batteries. When long-term operation of a large number of electronic devices in dispersed locations is required, energy harvesting has the advantages of outstanding longevity, relatively little maintenance, minimal disposal and contamination.

When two materials, at least one of which is non-conducting, come into contact with each other, a chemical bond, known as adhesion, is formed between the two materials. Depending on the triboelectric properties of the materials, one material may "capture" some of the electrons from the other material. If the two materials are separated from each other, a charge imbalance will occur. The material that captured the electron will negatively charged and the material that lost an electron will be positively charged. This charge imbalance gives rise to what is sometimes referred to as "static electricity." The term "static" in this case is somewhat deceptive, as it implies a lack of motion when in reality motion is necessary for charge imbalances to flow. The spark one feels upon touching a door knob is an example of such flow.

The triboelectric effect is a type of contact electrification in which certain materials become electrically charged after they come into contact with another such as through friction. It is the mechanism through which static electricity is generated. The triboelectric effects associated electrostatic phenomena are the most common electrical phenomena in daily life, from walking to driving. However, the triboelectric effect has been largely ignored as an energy source for electricity. Some electrostatic micro-generators have been developed and used in research relating to micro-electromechanical systems (MEMS), but such designs rely on an extra voltage source to charge electrode plates instead of harnessing triboelectric effect, leading to complicated structures and fabrication processes.

Previously demonstrated triboelectric generators require periodic contact and vertical separation of two materials that have opposite triboelectric polarities, making it only applicable to harvest energy from intermittent impact or shock. Such systems typically include a cavity with a constantly changing volume, which makes packaging difficult and

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limits applications in atmospheres with high humidity, corrosive chemicals or gases, and in water or other liquids.

Therefore, there is a need for a reliable, small and easily manufactured system for harvesting triboelectric energy that does not require a cavity therein.

SUMMARY OF THE INVENTION

The disadvantages of the prior art are overcome by the present invention which, in one aspect, is a generator that includes a first member, a second member and a sliding mechanism. The first member includes a first electrode and a first dielectric layer affixed to the first electrode. The first dielectric layer includes a first material that has a first rating on a triboelectric series. The second member includes a second material that has a second rating on the triboelectric series that is different from the first rating. The second member includes a second electrode. The second member is disposed adjacent to the first dielectric layer so that the first dielectric layer is disposed between the first electrode and the second electrode. The sliding mechanism is configured to move the first member laterally against the second member in a first direction, thereby generating an electric potential imbalance between the first electrode and the second electrode.

In another aspect, the invention is a method of generating electricity, in which a first member is placed against a second member. The first member includes: a first electrode and a first dielectric layer affixed to the first electrode the first dielectric layer including a first material that has a first rating on a triboelectric series. The second member includes a second material that has a second rating on the triboelectric series that is different from the first rating. The second member also includes a second electrode. The second member is disposed adjacent to the first dielectric layer so that the first dielectric layer is disposed between the first electrode and the second electrode. The first member is slid laterally against the second member along a first direction so that when at least a portion of the first member has slid apart from at least a portion of the second member, an electric potential imbalance occurs between the first electrode and the second electrode.

These and other aspects of the invention will become apparent from the following description of the preferred embodiments taken in conjunction with the following drawings. As would be obvious to one skilled in the art, many variations and modifications of the invention may be effected without departing from the spirit and scope of the novel concepts of the disclosure.

BRIEF DESCRIPTION OF THE FIGURES OF
THE DRAWINGS

FIGS. 1A-1D are a series of schematic diagrams one embodiment of a triboelectric generator.

FIG. 2A is a perspective view of an embodiment of a grooved triboelectric generator.

FIG. 2B is a perspective view of an embodiment of a grooved triboelectric generator in which the first member is separated from the second member.

FIG. 2C is a schematic diagram showing a portion of a triboelectric generator employing a nanowire structures.

FIGS. 3A-3D are a series of schematic diagrams showing electric generation using the embodiment shown in FIG. 2A.

FIGS. 4A and 4B are side elevational view of triboelectric generating devices employing two dielectric layers.

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FIG. 5 is a perspective view of a cylindrical embodiment of a grooved triboelectric generator in which the grooves run along a cylindrical axis.

FIG. 6 is a perspective view of a cylindrical embodiment of a grooved triboelectric generator in which the grooves run transverse to a cylindrical axis.

FIG. 7 is a perspective view of a disc-shaped embodiment of a grooved triboelectric generator in which the grooves extend radially from a central axis.

FIG. 8 is a schematic diagram showing dimensions of a triboelectric generator used in analysis thereof.

DETAILED DESCRIPTION OF THE INVENTION

A preferred embodiment of the invention is now described in detail. Referring to the drawings, like numbers indicate like parts throughout the views. Unless otherwise specifically indicated in the disclosure that follows, the drawings are not necessarily drawn to scale. As used in the description herein and throughout the claims, the following terms take the meanings explicitly associated herein, unless the context clearly dictates otherwise: the meaning of “a,” “an,” and “the” includes plural reference, the meaning of “in” includes “in” and “on.”

Related U.S. patent application Ser. No. 13/598,132, filed on Aug. 29, 2012 by Wang et al. and Ser. No. 14/032,864, filed on Sep. 20, 2013 by Wang et al. disclose methods of making triboelectric generators and components thereof and are both incorporated herein by reference for the purpose of disclosing such methods.

The present invention includes a triboelectric nanogenerator (TENG) that converts small-scale mechanical energy into electricity by sliding two surfaces laterally against each other. The principle of the TENG is based on sliding electrification between two surfaces, which expands the applicability of the TENG for diverse forms of mechanical motions.

As shown in FIGS. 1A-1D, a basic sliding embodiment of a TENG 100 includes a first member 110 disposed oppositely from a second member 120. The first member 120 includes a first electrode 112 and a first dielectric layer 114 coupled thereto. The second member 120 can serve as both a contact surface and an electrode. In one embodiment, the second member 120 can simply include a layer of aluminum (or other conductive material that is at a different position on a triboelectric series than the first dielectric layer 114), the first dielectric layer 114 can include a PTFE film and the first electrode 112 can include a metal, such as copper. The first electrode 112 may be coupled to the second electrode 120 through a load 130. (While not shown in FIGS. 1A-1D for the sake of simplicity, both the first member 110 and the second member 120 may each be mounted on a suitable substrate, such as an acrylic plate.) The first member and the second member do not have to be planar. They can be curved surfaces as long as they are parallel and have conformal contact with each other.

When the first dielectric layer 114 is placed against the second member 120, as shown in FIG. 1A, the triboelectric effect causes electrons to be transferred from the second member 120 to the first dielectric layer 114, thereby causing a net negative charge in the first dielectric layer 114 and a net positive charge in the second member 120. As the first member 110 is in contact with the second member 120 over their entire surfaces, the charges are balanced out. However, when a lateral force is applied to the second member 120 causing it to slide away from the first member 110, as shown

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in FIG. 1B, then the extra electrons in the first dielectric layer 114 stay in place due to the charge immobility associated with a dielectric while positive charges in the second member 120 move away from the first dielectric layer 114, causing a potential imbalance between the first member 110 and the second member 120. This then causes electrons to flow from the first electrode 112 through the load 130 to the second member 120. When the second member 120 is slid at its maximum offset from the first member 110, as shown in FIG. 1C, all of the negative charges held by the first dielectric layer 114 are balanced with corresponding positive charges in the first electrode 112 while the second member 120 is electrically neutral.

When the second member 120 is slid back over the first member 110, as shown in FIG. 1D, electrons flow back from the first electrode 112 through the load 130 into the second member 120, thereby more closely balancing the charges with the first dielectric layer 114. This causes a current to flow through the load 130 in an opposite direction from the direction it flowed during the motion shown in FIG. 1B. Once the second member 120 returns to the position shown in FIG. 1A, the charges are again balanced between the first dielectric layer 114 and the second member 120. (The same would hold true if the first member 110 is slid over the second member 120, or if both members are in motion so that there is relative sliding motion between the two members.)

The cycle shown in FIGS. 1A-1D can repeat itself, thereby generating an alternating current, if the TENG 100 is adapted with a sliding mechanism to receive force from a reciprocating motion source. The force can be directly applied, or it can be an inertial force due to acceleration. For example, the reciprocating motion source could be the repetitive footfalls of a person walking, or wave motion, or motion coming from a biological system—such as a heart-beat, or gusting wind, or one of many other types of repetitive motion.

One experimental embodiment of a TENG has a structure in which two contacting surfaces that can slide smoothly with one against the other. Acrylic was selected as a substrate material due to its decent strength, light weight and good machinability. On one substrate, aluminum thin film plays dual roles of an electrode and a sliding surface. On the other substrate, copper electrode is sandwiched between the substrate and a PTFE film. The PTFE film acts as another sliding surface. At its original position, the two sliding surfaces are fully aligned, with one sitting freely on the other. Driven by a tangential force applied to a substrate, relative displacement in contact mode occurs in lateral direction. After the two surfaces are fully displaced, the reciprocating force retraces them back to the aligned position.

The principle of the TENG is explained by the coupling between triboelectric effect and electrostatic effect. Once the PTFE film is brought into contact with the aluminum thin film, surface charge transfer takes place due to the triboelectric effect or contact electrification. Since PTFE is much more triboelectrically negative than aluminum, electrons are injected from aluminum into PTFE. At the aligned position, though triboelectric charges present on the surfaces, positive ones on aluminum are fully compensated by the negative ones on PTFE, producing no electric field in the surrounding space if the electric field at the edge is ignored. Once a relative displacement is introduced by an externally applied force in the direction parallel to the surfaces, triboelectric charges are not compensated at the displaced/mismatched areas, resulting in the creation of an effective dipole polar-

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ization parallel to the direction of the displacement. Therefore, the uncompensated charges generate electric potential difference (EDP) across the two electrodes. If the electric potential of the copper electrode is set to be zero, the EDP can be analytically expressed as a function of the displacement under simplified approximations.

$$\begin{aligned} EPD &= U_{Al} - U_{Cu} \\ &= \frac{q}{2\pi\epsilon_0 WL} \int_0^l \tan^{-1}\left(\frac{l}{t}\right) dt \\ &= \frac{q}{2\pi\epsilon_0 WL} \left[\frac{l}{2} \ln(t^2 + l^2) + \pi \tan^{-1}\left(\frac{l}{t}\right) \right] \end{aligned} \quad (1)$$

where l is the mismatched displacement between the two sliding plates, q is the quantity of the triboelectric charges on one plate, ϵ_0 is the vacuum permittivity, L is the length of the TENG's plate, W is the width of the TENG, and t is the thickness of the PTFE film.

If the two electrodes are electrically connected, once displacement is established, the uncompensated negative triboelectric charges on PTFE will repulsively drive free electrons on the copper electrode to the aluminum electrode, neutralizing the positive triboelectric charges and leaving behind positive induced charges. The flow of induced electrons lasts until the displacement reaches the maximum. Based on assumptions made in the analytical model, the induced charges equal the triboelectric charges in quantity. Therefore, at fully displaced position, the positive triboelectric charges are completely balanced out by induced electrons, indicating no more current flow. As the displacement is diminished by the reciprocating force, the induced electrons flow back to the copper electrode until the fully aligned position is restored. Therefore, in the entire process, alternating current (AC) is produced through the external load.

To characterize the performance of an TENG with a plate size of 6.4 cm by 3.8 cm, the short-circuit current (I_{sc}) and open-circuit voltage (V_{oc}) were measured at an average sliding velocity of 0.6 m/s introduced by a linear motor. It was found that the I_{sc} exhibits peaks of alternating directions. Increasing displacement gives a positive current peak, while shrinking displacement leads to a negative one. No electric current is produced at either aligned or entirely displaced position. The V_{oc} switches between zero and a maximum value, which corresponds to the aligned and fully displaced positions, respectively. Enabled by a full-wave diode bridge, the AC electric output can be rectified to a DC signal. With a diode bridge, the total accumulative induced charges, independent of sliding direction, can be added up. In this embodiment, every step represents an output current resulting from a one-way sliding motion, generating 0.6 μC of induced charges on average. Correspondingly, the area density of the triboelectric charges is calculated to be 257 $\mu\text{C}/\text{m}^2$.

In an experimental embodiment of such a dielectric-dielectric system, the sliding-triboelectric nanogenerator includes two plates (71 mm \times 50 mm) with glass slides as the supporting substrates to ensure the surface flatness. Polyamide 6,6 (Nylon) and polytetrafluoroethylene (PTFE) films, the two polymers at the opposite ends of the triboelectric series, are chosen as the triboelectric layers adhered on surfaces of the glass slides for effective electrification during sliding. On each polymer film, a layer of metal electrode was deposited on the side next to the glass slide (named as top electrode for the one on Nylon and bottom

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electrode for the one on PTFE). The two plates are kept in parallel to each other and the polymeric surfaces are in intimate contact. As driven by the mechanical motion/vibration along the long-edge of the plate, the two plates slide against each other, with the contact area changing periodically. In order to enhance the triboelectric charge density on the surface, the PTFE film was dry-etched using inductive coupled plasma (ICP) to create aligned nanowire-structures, which increase the surface roughness and the effective surface area. The PTFE surface is uniformly covered with nanowire-structures, with an average length of $\sim 1.5 \mu\text{m}$. The PTFE-covered plate was bonded to a stationary stage, while the Nylon side was fastened to a parallel flat-end rail guide, which was connected to a linear motor for inducing an in-plane sliding motion.

In this embodiment, the triboelectrification will leave the Nylon surface with net positive charges and the PTFE with net negative charges with equal density. Since the tribocharges on the insulators will only distribute in the surface layer and will not be leaked out for an extended period of time, the separation between the positively-charged surface and negatively-charged surface is negligible at this overlapping position, and thus there will be little electric potential drop across the two electrodes. Once the top plate with the positively-charged surface starts to slide outward, the in-plane charge separation is initiated due to the decrease in contact surface area. The separated charges will generate an electric field pointing from the right to the left almost parallel to the plates, inducing a higher potential at the top electrode. This potential difference will drive a current flow from the top electrode to the bottom electrode in order to generate an electric potential drop that cancels the tribocharge-induced potential. Because the vertical distance between the electrode layer and the tribo-charged polymeric surface is negligible compared to the lateral charge separation distance, the amount of the transferred charges on the electrodes approximately equals the amount of the separated charges at any sliding displacement. Thus, the current flow will continue with the continuation of the on-going sliding process that keeps increasing the separated charges, until the top plate fully slides out of the bottom plate and the tribo-charged surfaces are entirely separated.

Subsequently, when the top plate is reverted to slide backwards, the separated charges begin to get in contact again but no annihilation due to the insulator nature of the polymer materials. The redundant transferred charges on the electrodes will flow back through the external load with the increase of the contact area, in order to keep the electrostatic equilibrium. This will contribute to a current flow from the bottom electrode to the top electrode, along with the second half cycle of sliding. Once the two plates reach the overlapping position, the charged surfaces get into fully contact again. There will be no transferred charges left on the electrode, and the device returns to the initial state in. In this entire cycle, the processes of sliding outwards and inwards are symmetric, so a pair of symmetric alternating current peaks should be expected.

The model constructed here has the same structure and dimensions (71 mm \times 50 mm in surface) with the real device, and those two tribo-charged surfaces are assigned with a charge density of $\pm 70 \mu\text{C}/\text{m}^2$, respectively. The device is in open-circuit condition, which means no electron transfer between the two electrodes. When the two plates are in the fully aligned stacking position, there is no potential difference generated. When the top plate slides about half way out (with a displacement of 41 mm), there will be a 2950 V potential difference between the two electrodes; and this

potential difference will increase to 1.03×10^5 V when the top plate just slides out of touching the bottom plate (with a displacement of 71 mm). The voltage keeps increasing when the displacement gets larger, even after the plates slide out of each other. This is because the voltage is the path-integral of the electric field along the displacement. On the other hand, the amounts of transferred charges between the two electrodes under these different displacements are also simulated through equating the potential of the electrodes at the short-circuit condition. The amount of transferred charges increases linearly with the displacement before the top plate slides out of the bottom plate (with the displacement smaller than 71 mm). Different from the trend of the voltage, the amount of transferred charges will saturate at the total amount of tribo-charges on one surface after the plates have fully slid out of each other, because there is no further charge separation here. So, the effective displacement region for generating electricity is between 0 mm and 71 mm, where the contact area of the two plates is changed during the relative sliding of the two plates.

The electrical output of the sliding-TENG was measured, with one plate guided by the linear motor in the direction parallel to the long-edge of the plates. The sliding displacement was 71 mm, which was the same with the length of the plate and thus covered the entire effective region for generating electricity. The sliding movement was in a symmetric acceleration-deceleration mode, with the acceleration rate of ± 20 m/s². The open-circuit voltage (V_{OC}) was measured by an electrometer with very large input resistance. The electrode at the back of Nylon film was connected to the positive probe. When the plates in the TENG slid from the contact position to the separated position, the V_{OC} jumped from 0 to 1300 V, which reflects the induced potential difference between the two electrodes by the in-plane charge separation. At the separation position, the V_{OC} decayed a little bit, due to the slow charge leakage through the electrometer. When the TENG slid back to the contact position, the V_{OC} jumped back to 0. The density of the transferred charge ($\Delta\sigma$) was also measured at the short-circuit condition. Charges with a density of ~ 105 $\mu\text{C}/\text{m}^2$ transferred back and forth between the two electrodes, while the plates slid in and out. Since the plates got fully separated in each cycle, the transferred charge density should approximately equal to the triboelectric charge density on the polymeric surfaces. With these experimental results, the measured V_{OC} is smaller than the simulated potential difference, which is possibly due to the limitation of the electrical measurement system to record such a high voltage and the imperfection from the ideal open-circuit condition. The transfer of the charges between the electrodes in the outer circuits produced an alternating-current output, with the peak short-circuit current density (J_{SC}) of 4.1 mA/m² at a maximum sliding velocity of 1.2 m/s. In this experimental embodiment, with such a power output converted from the sliding motion, hundreds of commercial light-emitting diodes (LEDs) were instantaneously driven by a single TENG device.

The TENG's effective output power to the loads depends on the match with the resistance of the load. When the resistance is below ~ 1 M Ω , the output current density and the voltage have little changes from the short-circuit condition: the current density remains at a value of J_{SC} while the voltage stays close to 0. This is because the TENG has infinitely-large inner resistance. When the resistance goes beyond 1 M Ω , the current density will drop with the increase of the resistance; while the voltage on the load increases. Consequently, the instantaneous power density on the load

remains close to 0 with the resistance below 1 M Ω , and reaches the maximum value of 0.42 W/m² at a resistance of ~ 50 M Ω . This is the maximum output power density on the device.

The output of the planar-sliding-driven TENG is directly determined by the parameters of the sliding motion—the displacement and the velocity, because the flow of electricity originates from the tribo-charge separation under sliding. As simulated, before the two plates fully slide out of each other (with a displacement smaller than 71 mm), the voltage increases monotonically with the displacement. Also, if there is a uniform tribo-charge distribution on the polymeric surface, the total amount of transferred charges will have a linear relationship with the displacement, which can be expressed in charge density as:

$$\frac{\Delta\sigma}{\sigma_0} = \frac{\Delta L}{L_0} \quad (2)$$

where $\Delta\sigma$ is the transferred charge density, σ_0 is the tribo-charge density on the polymeric surface, ΔL is the sliding displacement and L_0 is the length of the plate which is 71 mm. According to the definition of current density (J), it has the following relationship:

$$J = \frac{d\Delta\sigma}{dt} \quad (3)$$

where t is the time. Merging equation (2) into (3) results in

$$J = \frac{\sigma_0}{L_0} \cdot \frac{d\Delta L}{dt} = \frac{\sigma_0}{L_0} v \quad (4)$$

where v is the instantaneous velocity of the sliding. So, the current density should be proportional to the instantaneous velocity at which the two plates are being separated.

A systematic study of these relationships between the electrical outputs (V_{OC} and J_{SC}) and the sliding conditions was carried out experimentally. In the first group of experiments, the electrical outputs were measured under a series of 7 different sliding displacements from 11 mm to 71 mm, with an acceleration kept at 20 m/s². It was found that, the V_{OC} increases with the displacement, which is in accordance with simulation results. The measured transferred charge density $\Delta\sigma$ displays a linear relationship with the displacement, which can be linearly fitted with the correlation coefficient of 0.981. As for the peak value of J_{SC} which is in proportional to the maximum velocity v_m , it also has a positive correlation with the displacement. This is because v_m has such a relationship with the displacement:

$$v_m = \sqrt{a\Delta L} \quad (5)$$

where a is the acceleration and ΔL is the total displacement (the displacement for each acceleration and deceleration process is $\Delta L/2$, respectively).

When the sliding displacement remains at a constant value of 71 mm, the maximum velocity of the sliding is solely determined by the acceleration. Thus, the acceleration was varied to investigate the velocity's influence on the output. It was found that V_{OC} has very little increase with the rising acceleration, which is also consistent with the theoretical expectation that V_{OC} is only determined by the displacement. However, the changing rate of the voltage will

depend on the sliding velocity. The higher the velocity, the faster the voltage increases/decreases in sliding. As for the output current, the peak value of J_{SC} gets larger at higher acceleration, because of the larger maximum velocity in sliding. However, the sliding velocity has no influence on the transferred charge density $\Delta\sigma$ under the constant displacement.

Because the essence in the working mechanism of the sliding-TENG is the cycled switching between the separation and full contact of the opposite tribo-charges, there should be little electricity generated in the following two cases: (1) If the sliding motion does not result in the change of the contact area between two plates, for example, if a smaller plate slides inside the perimeter of a larger plate at all time, then little output can be measured. This is because there is no polarization generated in this case. (2) If the two plates do not fully in tight contact with each other at the overlapping position, there is always a vertical gap distance between them, which results in two cases: the first is that little triboelectric charges are generated; the second case is that if there are triboelectric charges on the plates, the gap between them in the vertical direction quickly decays the strength of electrostatic interaction, resulting in a reduced output. When the vertical distance between the two plates of the TENG is gradually increased from 0 to 2 mm, the output voltage, current and transferred charges all quickly decay to zero.

The planar sliding mode TENG disclosed herein has several advantages, including: (1) This TENG design does not need a gap between the two plates. Thus it will be unnecessary to have elastic supporting components (such as springs) between the two plates to ensure the effective charge separation. This brings up a lot of convenience in packaging the TENG device; (2) there is no need for a large amount of mechanical energy input to trigger this TENG design, which can help to improve the energy harvesting efficiency. The mechanical energy only needs to overcome the work done by the sliding friction between the two plates. (3) This TENG design is simple in structure, easy in fabrication, compact in volume, stable in performance, cost-effective and robust. With these advantages, such in-plane charge-separation-based TENGs can harvest mechanical energies in the form of relative sliding that are supplied by many different working configurations, for example, the relative rotation of two contacting plates, the vibration of the piston, the rotation of the axis to its tube, and so on. Besides, those types of mechanical energy that can drive the relative sliding between two objects can also be harvested using this principle of in-plane charge-separation-based TENG, which can greatly expand the application of this type of TENG to scavenge mechanical energy from wind power, oceanic wave, human activities, and so on.

As shown in FIGS. 2A, 2B and 3A-3D, the first dielectric layer 214 can include a first grating of evenly spaced apart parallel ridges 216 and troughs 218. Similarly, the second member can include a second grating first grating of evenly spaced apart parallel ridges 226 and troughs 228. As can be seen in FIGS. 3A-3D, while the overall surface contact area density of this embodiment is essentially one half that of the embodiment shown in FIG. 1A-1D, the total sliding distance necessary for maximum charge transfer is limited to the width of a single ridge. Thus, depending on the width of the ridges (which can be microscale using lithographic techniques), this embodiment can generate its maximum current with an extremely small scale source of reciprocal motion (such as vibrations). These embodiments can be made using well known thin film application processes for applying

layers to the substrates and standard lithographic techniques for etching the troughs. As shown in Fig. 2C, aligned nanowire-structures can be added to increase the surface roughness and the effective surface area. As discussed above, in one embodiment, the nanowire-structures can have an average length of about 1.5 μm .

As shown in FIG. 4A, one embodiment includes: a first member 310 having a first electrode 312 mounted on a first rigid substrate 330 and a first dielectric layer 314 applied thereto, and a second member having a second electrode 324 mounted on a second rigid substrate 332 and a second dielectric layer 322 mounted thereto. As shown in FIG. 4B, a two dielectric layer embodiment can also include gratings formed in the first dielectric layer 314 and the second dielectric layer 322.

Introducing linear grating on the sliding surfaces enables the new principle to become an extremely efficient means for energy harvesting; and it is far superior to the previously demonstrated ones in total output charge, current frequency and efficiency. A linear grating with a uniform period is fabricated on both sliding surfaces. The rows of the grating units have the same size as intervals in between, with all rows being electrically connected at both ends by two buses. The grating patterns on both sliding surfaces are identical so that they can match well with each other when aligned. Although the grating design reduces the total contact area by half thus seemingly sacrifices half of the triboelectric charges, it increases the percentage of the mismatched area to 100% for a displacement of only a grating unit length rather than the entire length of the TENG so that it dramatically increases the transport efficiency of the induced charges. Induced free electrons can be pumped back and forth between electrodes for multiple times due to the grating structure, providing multi-folds of output charge compared to a non-grating TENG. Every row of the grating units can be considered as a reduced-sized TENG having a parallel connection with all other rows through buses. In contrast to a non-grating TENG that needs to be fully displaced in order to complete pumping of the induced charges for one time, the grating TENG only requires a displacement of a unit length to completely transport the induced charges, largely improving the energy conversion efficiency. With further displacement of another length of the unit, back flow of the induced charges can be realized. Therefore, for a one-way sliding process across the whole length of the TENG, the induced charges can be pumped for $(2N-1)$ times in total, where N is the number of grating units. If we take into account that the contacting area decreases as the two surfaces slide apart, the following equation represents the total induced charges Q that the grating TENG can provide for a single sliding across the entire length of the TENG:

$$\begin{aligned} Q &= Nq' + |-q' \times (N-1)| + q' \times (N-1) + \dots + |-q'| + q' \\ &= Nq' + 2q' \times \sum_{i=1}^{N-1} i \\ &= (2q'N)N/2 \end{aligned} \quad (6)$$

where q' is the induced charges generated from a single grating unit for a displacement of the unit length.

The total maximum induced charges generated by a non-grating TENG can be equivalently expressed as $2q'N$. Therefore, Eq. (6) indicates that the total induced charges

linearly increase with the grating density. Experimental data from grating TENGs with more units further confirm the validity of the theoretical analysis.

Though the experimental data closely match the theoretical values for $N \leq 4$, slight deviation starts to appear if N further increases. The deviation may be attributed to two probable reasons. The first is non-ideal orientation mismatch. The two sliding surfaces are likely to have an angle of mismatch that is introduced by experimental operation. As the length of the grating units shrinks, the angle of mismatch will exert more substantial effect on the effective contact area between the two surfaces, leading to increasingly reduced output charge. This effect can be largely eliminated by more precise alignment during experiment operation. Secondly, assumptions made in the analytical theory may become imprecise for very fine grating units due to the edge effect of each unit. The assumption of infinite charged plane will no longer hold once the grating edges can dominantly affect the electric field distribution, leading to reduced quantity of induced charges. Further systematic investigation by both experiment and simulation is required to quantitatively understand this non-ideal effect. As experimentally observed, V_{oc} is only weakly related to the number of grating units, though slight reduction can be observed. The reduction can also be attributed to the increasingly stronger effect from the mismatched angle. Besides, finer grating units will theoretically give a smaller V_{oc} , though this effect may be dominant only when the grating unit has a length approaching the PTFE's thickness. The advantages of the grating structure include not only the enhanced total transported charges but also improved output current. With constant sliding velocity, finer grating shortens the time to transport induced charges between the electrodes for one time, resulting in higher output current. However, the peak of I_{sc} does not increase linearly with the number of units, which may result from non-uniform velocity during sliding process.

To demonstrate the capability of the new principle as a direct power source, a total of 80 commercial LED bulbs were utilized as operating load. They were divided into two groups, which were connected to a TENG with reversed polarity in order to clearly demonstrate the AC output without rectification. One substrate of the TENG was fixed on a breadboard where the LEDs were installed, while the other one was attached to human fingers. As the hand swept back and forth, the sliding was realized. It was noticed that faster sweeping generated higher current peaks as compared with those from slower sweeping. Due to the AC output, the two LED groups were alternately lighted up, as indicated by "ON" and "OFF" states.

Besides the planar design, other configurations include, concentric discs having relative rotation and coaxial tubes having either rotational motion or reciprocating piston motion. The principles demonstrated for the grating TENG can be applied to other configurations. For example, as shown in FIG. 5, in one embodiment of a TENG 400 the first member 410 and the second member 420 are cylindrical. The first dielectric layer 414 includes a first grating of evenly spaced apart parallel ridges 416 and troughs 418 and the second member 420 includes a second grating of parallel ridges 426 and troughs 428. All of the ridges and troughs extend parallel to the axis of the cylinder. Thus, when either the first member 410 or the second member 420 is rotated about the cylindrical axis (or both rotated so long as there is relative motion between them), the ridges of the second member 420 and the first member 410 will come in and out of contact. This embodiment is effective when it is desired

to turn rotational motion into electricity. In the embodiment shown in FIG. 6, the ridges 516 and troughs 518 of the first grating and the second grating are disposed circumferentially about the cylinder and the sliding mechanism is configured to apply reciprocating motion along the cylindrical axis to either the first member 510 or the second member 520 (or both so long as there is relative motion between them), thereby converting the reciprocating motion into electricity. In the embodiment shown in FIG. 7, the ridges 616 and troughs 618 of the first grating and the second grating extend radially outwardly from a central axis of a disk. Electricity is generated when at least one of the first member 610 and the second member 620 is caused to rotate around the central axis of the disks (or both can be rotating so long as there is relative rotational motion between them).

An analytical model for calculating the open-circuit voltage of a TENG 700 is now presented using the diagram shown in FIG. 8. For simplicity of the mathematical derivation, the analytical model is built based on the following assumptions:

(1) The two sliding surfaces of the TENG are infinitely large because the lateral dimension is much larger than the vertical thickness.

(2) The generated triboelectric charges, which are non-mobile and non-annihilative, are uniformly distributed on the two surfaces. This is an excellent approximation if the two materials are insulative. In a case that one side is metal, this approximation is made for easy derivation.

(3) Both the aluminum and the PTFE thin film can be simplified as planar surfaces which retain their shapes instead of having deformation when sliding laterally. Once the two surfaces contact with each other, triboelectric charges are created due to contact electrification. Based on assumption (2) and assumption (3), the lateral displacement l brings about uncompensated positive and negative triboelectric charges in the displaced areas on the upper surface and the lower surface, respectively.

If we define the electric potential of the copper electrode (U_{Cu}) to be zero, the open circuit voltage of the TENG is equal to the electric potential of the electrode electrode (U_{Al}), that is,

$$V_{OC} = U_{Al} - U_{Cu} = U_{Al} = U_{P1} - U_{P3} \quad (S1)$$

Also, the electric potential difference can be expressed as

$$U_{P1} - U_{P3} = \int_{P1}^{P3} E \cdot dl_{1 \rightarrow 3} = \int_{P1}^{P2} E_{1 \rightarrow 2} \cdot dt + \int_{P2}^{P3} E_{2 \rightarrow 3} \cdot dt \quad (S2)$$

Meanwhile, given assumption (1) and (2), we can consider the upper surface as charged plate of infinity in size, so that the electric lines of force are perpendicular to the surface of the plate as well as the patch from P_2 to P_3 . As a result

$$\int_{P2}^{P3} E_{2 \rightarrow 3} \cdot dt = 0 \quad (S3)$$

and

$$U_{Al} = \int_{P1}^{P2} E_{1 \rightarrow 2} \cdot dt \quad (S4)$$

In order to calculate the electric field strength $E_{1 \rightarrow 2}$ in the path from P_1 to P_2 , let us consider an infinite, charged line

in the displaced area on the upper surface. And the corresponding electric field strength E_{st} at P_2 can be quantitatively expressed as

$$E_{st} = \int_{-\theta}^{+\theta} \frac{\sigma}{4\pi\epsilon_0} \cdot \frac{\cos\theta}{\sqrt{l^2 + l^2}} \cdot d\theta = \frac{\sigma}{2\pi\epsilon_0} \cdot \frac{\sin\theta}{\sqrt{l^2 + l^2}} \quad (S5)$$

where ϵ_0 is the permittivity of vacuum, t is the thickness of the PTFE film, l is the displacement, and σ is the line charge density

$$\sigma = \frac{q}{WL} \quad (S6)$$

where q is the total triboelectric charges, W and L are the width and length of the two sliding surfaces, respectively. Meanwhile, in our case, compared with the PTFE's thickness, the charged line is considered to be infinitely long, thus,

$$\theta = 90^\circ \quad (S7)$$

Upon combination and simplification, E_{st} can be expressed as

$$E_{st} = \frac{q}{2\pi\epsilon_0 WL \sqrt{(l^2 + l^2)}} \quad (S8)$$

However, only the component along Z axis of the electric filed strength E_{st} is parallel to the electric field, making the effective electric filed strength expressed as

$$E_{eff} = E_{st} \cdot \sin\beta \quad (S9)$$

$$\sin\beta = \frac{t}{\sqrt{l^2 + l^2}} \quad (S10)$$

Upon combination and simplification,

$$E_{eff} = E_{st} \cdot \sin\beta = \frac{q}{2\pi\epsilon_0 WL} \cdot \frac{t}{(l^2 + l^2)} \quad (S11)$$

Thus, the total electric filed strength $E_{1 \rightarrow 2}$ generated at P_2 along the z -axis by the triboelectric charges on the entire displaced area of the upper surface can be calculated as

$$E_{1 \rightarrow 2} = \int_0^l \frac{q}{2\pi\epsilon_0 WL} \cdot \frac{t}{(l^2 + l^2)} dt = \frac{q}{2\pi\epsilon_0 WL} \cdot \tan^{-1}\left(\frac{l}{l}\right) \quad (S12)$$

Submit the Equation (S12) into the Equation (S4)

$$U_{At} = \int_0^l E_{1 \rightarrow 2} \cdot dt = \int_0^l \frac{q}{2\pi\epsilon_0 WL} \cdot \tan^{-1}\left(\frac{l}{l}\right) dt \quad (S13)$$

Finally, the open-circuit voltage V_{oc} between the two electrodes can be expressed as

$$V_{oc} = U_{At} = \frac{q}{2\pi\epsilon_0 WL} \cdot \left[\frac{l}{2} \ln(l^2 + l^2) + l \tan^{-1}\left(\frac{l}{l}\right) \right] \quad (S14)$$

The energy conversion efficiency ($\eta\%$) can be estimated through the conversation of energy. According to the definition:

$$\eta\% = \frac{E_{ele}}{E_{Mech}} \times 100\%$$

where E_{ele} is the electrical energy generated in the half cycle of the displacement, and E_{Mech} is the mechanical energy input. They can be estimated as follow.

The maximum electrical energy generated by the sliding TENG in a half-cycle, be estimated using the data of the TENG's output characteristic when driving external load. The highest power output is reached at the resistance of 80 M Ω , which will correspond to the maximum electric energy output (E_{ele}). It can be calculated according to the following equation:

$$E_{ele} = \int I^2 R dt$$

The curve of $I^2 R$ vs. t ($R=80$ M Ω) can be derived from the corresponding I vs. t curve, and through the integration of one ($I^2 R$) peak in a half-cycle, we can get:

$$E_{ele} = 0.145 \text{ mJ.}$$

In general, the mechanical energy input for driving the sliding TENG is converted into two parts: the electrostatic energy (E_{es}) of the two oppositely-charged plates at the fully displaced position, and the electrical energy (E_{ele}) the TENG generated in the sliding process.

As for the electrostatic energy E_{es} , it can be estimated as:

$$E_{es} = U_T \sigma_0 A + U_B (-\sigma_0) A = (U_T - U_B) \sigma_0 A = V_{OC} \sigma_0 A$$

where U_T and U_B are the potentials at the top plate and bottom plate, respectively; and A is the area of the plate, which is 35.5 cm². In this estimation, we assume each charged plane has a uniform potential, which is reasonable as shown in the simulated results of the potential distribution. From the electrical measurement of the TENG, V_{OC} is ~1300 V and σ_0 is ~105 $\mu\text{C}/\text{m}^2$. Thus, we can get

$$E_{es} = V_{OC} \sigma_0 A = 1300 \text{ V} \times 105 \times 10^{-6} \times 35.5 \times 10^{-4} \text{ C} = 0.485 \text{ mJ}$$

Thus, the mechanical energy input E_{Mech} can be estimated to be:

$$E_{Mech} = E_{es} + E_{ele} = 0.630 \text{ mJ}$$

The other part of energy input is the heat dissipated during mechanical sliding, which is rather difficulty to estimate for the current design. If we ignore this component, the maximum energy conversion efficiency can be estimated as follows:

$$(\eta\%)_{\max} = \frac{E_{ele}}{E_{Mech}} \times 100\% = \frac{0.145 \text{ mJ}}{0.630 \text{ mJ}} \times 100\% = 23.0\%$$

While many different materials can be organized according to a triboelectric series, the following is one representative example of a triboelectric series:

Asbestos
Glass
Mica
Nylon
Lead
Silk
Aluminum
Steel
Wood
Lucite
Amber
Hard Rubber

- Mylar
- Nickel
- Copper
- Silver
- Brass
- Synthetic Rubber
- Gold, Platinum
- Sulfur
- Acetate, Rayon
- Polyester
- Celluloid
- Polystyrene
- Orlon, Acrylic
- Polyvinylidene chloride (Saran)
- Polyurethane
- Polyethylene
- Polypropylene
- Polyvinylchloride (Vinyl)
- PTFE
- Silicon
- Teflon
- Silicone Rubber

The above described embodiments, while including the preferred embodiment and the best mode of the invention known to the inventor at the time of filing, are given as illustrative examples only. It will be readily appreciated that many deviations may be made from the specific embodiments disclosed in this specification without departing from the spirit and scope of the invention. Accordingly, the scope of the invention is to be determined by the claims below rather than being limited to the specifically described embodiments above.

What is claimed is:

1. A generator, comprising
 - (a) a first member, including:
 - (i) a first electrode; and
 - (ii) a first dielectric layer affixed to the first electrode, the first dielectric layer including a first material that has a first rating on a triboelectric series, the first dielectric layer including a first grating of evenly spaced apart ridges and troughs, each of the ridges and each of the troughs having a common width;
 - (b) a second member that includes a second material that has a second rating on the triboelectric series that is different from the first rating, the second member

including a second electrode, the second member disposed adjacent to the first dielectric layer so that the first dielectric layer is disposed between the first electrode and the second electrode, the second member including a second grating of evenly spaced apart ridges and troughs, each of the ridges and each of the troughs having a common width so that the width of the troughs of the second member is equal to the width of the ridges of the first dielectric layer and so that the width of the ridges of the second member is equal to the width of the troughs of the first dielectric layer; and

(c) a sliding mechanism configured to cause lateral relative motion between the first member against the second member along a first direction, thereby generating an electric potential imbalance between the first electrode and the second electrode.

2. The generator of claim 1, further comprising:
 - (a) a first rigid substrate to which the first member is affixed; and
 - (b) a second rigid substrate to which the second member is affixed.
3. The generator of claim 1, wherein the first member is substantially planar and wherein the second member is substantially planar and parallel to the first member.
4. The generator of claim 1, wherein the first electrode comprises a metal, wherein the first dielectric layer comprises PTFE and wherein the second member comprises aluminum.
5. The generator of claim 1, wherein the second member further includes a second dielectric layer, the second dielectric layer having the second rating on the triboelectric series and disposed against the first dielectric layer.
6. The generator of claim 5, wherein the first dielectric layer comprises PTFE and wherein the second dielectric layer comprises nylon 6,6.
7. The generator of claim 1, wherein at least one of the first member and the second member includes a surface having a nanostructure texture extending therefrom.
8. The generator of claim 1, further comprising a load electrically coupled to the first electrode and to the second electrode.

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